

Direct Numerical Simulations of Multistage Ignition for a Stratified HCCI Engine with Exhaust Gas Recirculation : H₂O₂ Effect

Hossam A. El-Asrag* and Yiguang Ju

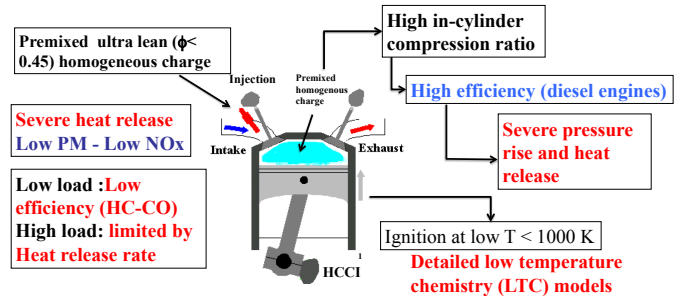
Department of Mechanical and Aerospace Engineering

Princeton University, Princeton, 08544 USA

*Tel: (001) 6507047090. Email: helasrag@princeton.edu

- Fossil fuels depletion and EPA regulations drive the need for:
 - Alternative synthetic fuels
 - Efficient engines with high pressure compression ratios
 - Burning in the lean premixed mode to reduce emissions
- Homogenous Compression Charge Ignition (HCCI) Engines auto-ignite a **homogenous lean premixed** charge at **high pressure compression ratios**

II-HCCI Operation and Challenges

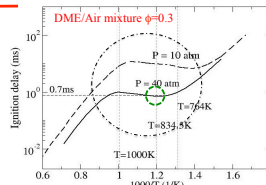
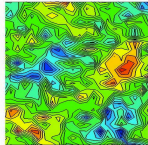


Not well understood (Objectives):

- Autoignition at low temperature with thermal/mixture stratification
- Effect of exhaust gas recirculation (EGR) on autoignition
- The coupling effect of transport/chemistry on LTC ignition

III-Numerical Setup : HCCI

Volumetric heating compression at the TDC - P=30 atm
T=834.5K (NTC)
DME/Air mixture
55 species (Curran et al. CNF 1998)



Domain: 1.5x1.5 mm domain
362x362 grid points (4 μm mesh)
Fully compressible formulation
Periodic in all directions

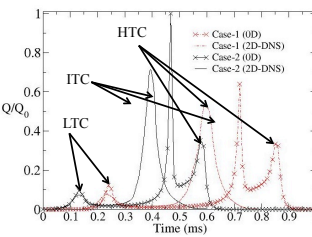
Initial H₂O₂ from EGR
Case-I Y_{H₂O₂}=0 Case-II Y_{H₂O₂}=400ppm

Initial spectrum conditions			
	Mean	rms	Integral length Scale
U	0	0.5	1.24 mm
T	834.5 K	15K	1 mm
φ	0.3	0.1	1 mm

Stratification in T and φ using P_a Y_{H₂O₂}=0 Y_{H₂O₂}=400ppm spectrum
Uncorrelated T and φ spectrum
Re_ρ=20
η=5.3μm

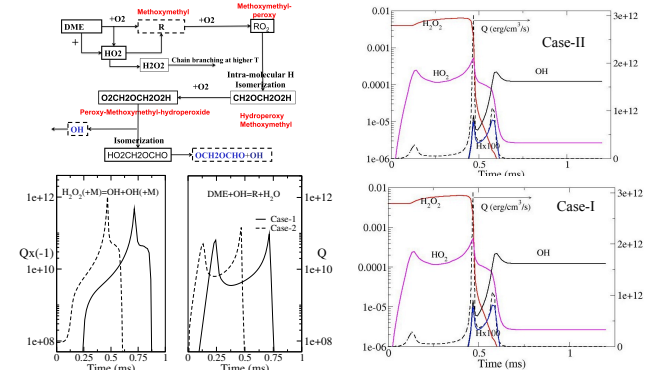
$$E(k) = \frac{32}{3} \sqrt{\frac{2}{\pi}} \frac{u'^2}{k_v} \left(\frac{k}{k_v}\right)^4 \exp\left[-2\left(\frac{k}{k_v}\right)^2\right]$$

IV-NTC Autoignition (OD/DNS)



- CONCLUSIONS-I**
- DME/Air has **three NTC ignition stages**
- Low TC, Intermediate TC, High TC
- H₂O₂ from EGR enhances autoignition by increasing the OH radical pool
- 46% reduction** in LTC ignition
- 34% reduction** in HTC and ITC ignitions

V-LTC chemistry and H₂O₂ Effect



$$t_{mix} = 1/D_T |\nabla \theta|^2, \theta = (T - T_{min}) / (T_{min} - T_{max})$$

$$t_{diff} = D_{IKI} / S_L^2$$

$$t_{chem} = \frac{C_{p,mix} T \rho}{Q}$$

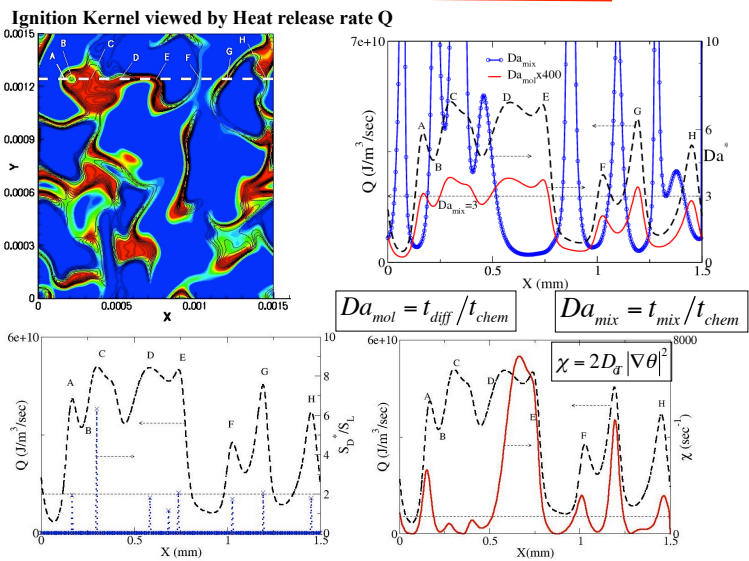
$$D_{IKI} = D_{OH} + D_{HO_2}$$

$$S_D = \frac{\left(\omega_{IKI} - \frac{\partial}{\partial x_i} \left(D_{IKI} \rho \frac{\partial Y_{IKI}}{\partial x_i}\right)\right)}{\rho_s |\nabla Y_{IKI}|}$$

VII-Conclusion

- DNSs are conducted for a stratified HCCI engine with EGR
- DME/air has three ignition stages in the NTC region initial conditions
- H₂O₂ addition from EGR accelerates ignition by the OH radical pool
- Thermal and mixture stratification introduce mixing time scales that interact strongly with chemistry after the LTC ignition stage
- Two different reaction front ignition modes are found : a homogeneous ignition and deflagration modes
- A criteria to distinguish between the different modes are developed based on the local time scales and radical pool

VI-Flame propagation Modes at LTC



Deflagration wave at flame front A, D,E,F,G, and H
Homogeneous spontaneous ignition at point C